


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## Enhancement of Sc and Ti extraction rates from Fe-depleted slag by hydrogen peroxide and sulfuric acid leaching

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# ENHANCEMENT OF Sc AND Ti LEACHING RATES FROM Fe REMOVED SLAGS

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## Abstract

Conditioning of bauxite residue for enhanced Sc and Ti leaching efficiencies was performed in this study. Acidic leaching conditions provided for higher Sc and Ti leaching also result in higher dissolved Fe in leachate. In order to tackle Fe interference, red mud is treated in electric arc furnace for prior Fe removal. Various smelting conditions such as cooling rate (20 °/min, 1400 °/min) and feeding lime (CaO) were performed to obtain slags with different crystallography and chemical properties. All slags were subjected to acidic leaching with 2.5 M hydrogen peroxide (H<sub>2</sub>O<sub>2</sub>): 2.5 M sulfuric acid (H<sub>2</sub>SO<sub>4</sub>) combination with a solid to liquid ratio of 1: 10 at 75 °C. Slags were analyzed in term of phase content, crystallinity and morphology by XRD and SEM analyses. Effect of various smelting conditions on leaching efficiencies and kinetics of Sc and Ti was investigated.

## Introduction

- Wide application area of Ti as metal, compound and alloys; exhausted primary resources
- Sc has limited primary sources and has to be extracted mainly from secondary raw materials or as a by-product of uranium, nickel-laterite or titanium pigment processing
- Red mud** is a very promising material to recover Ti and Sc
- High Fe amount in red mud decreases selectivity of Ti and Sc recovery and increases complexity of precipitation process
- Iron deficient slags, which were produced after electric arc furnace treatment of red mud, were subjected to acidic leaching in order to determine the most optimum slag chemistry and crystallinity.

## Methods and Materials

### Pyrometallurgical treatment



- Red mud (AoG)
- Reductant: Lignite coke (87% C)
- Flux: Lime (95% CaO)
- Smelting: 100kW EAF
- Batch mass: 2 kg
- T ≈ 1500°C
- Holding time ≈ 1 hour
- Cooling: quenched (water), ambient cooling (air)

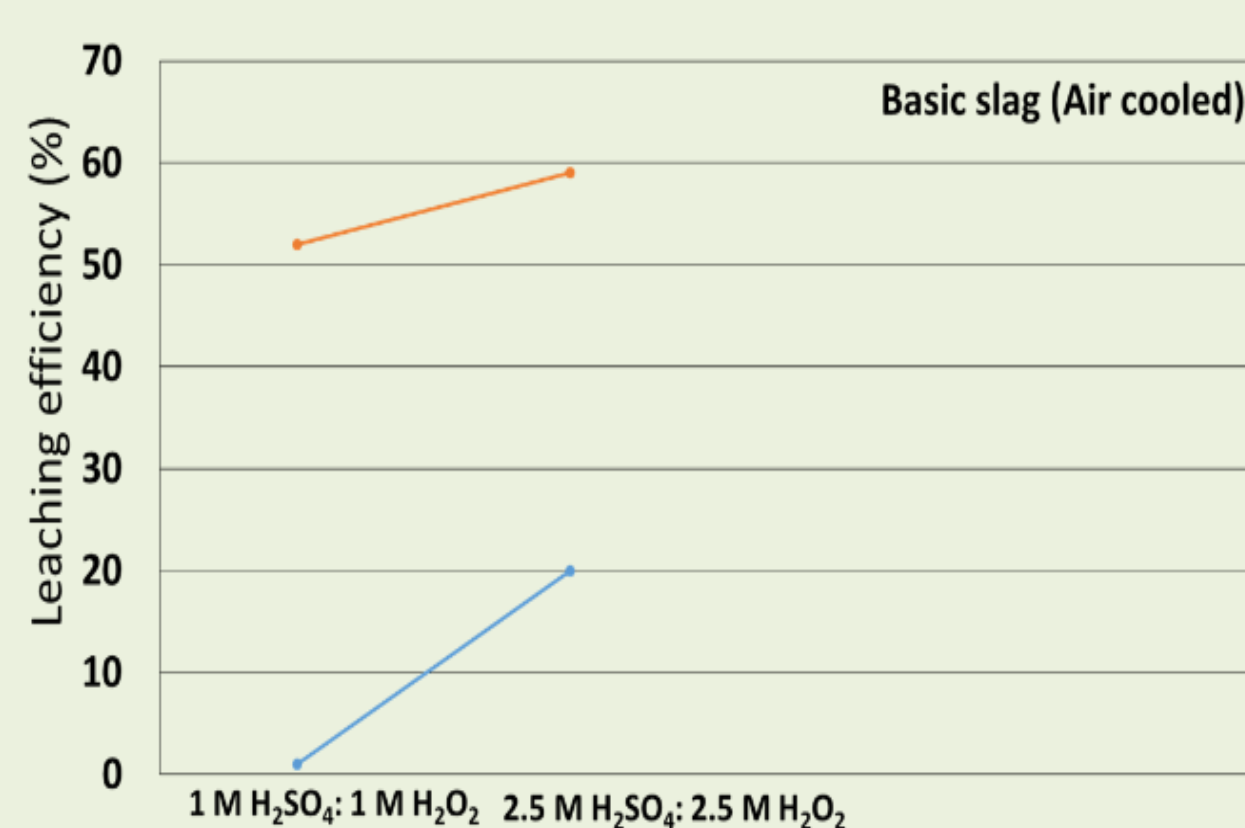
wt. %	Fe <sub>2</sub> O <sub>3</sub>	Al <sub>2</sub> O <sub>3</sub>	CaO	SiO <sub>2</sub>	TiO <sub>2</sub>	Sc (mg/kg)
Bauxite residue	43.5	24	10.2	5.5	5.6	130
Slag	1.8	38.3	43.2	7.6	7.6	170

### Hydrometallurgical treatment

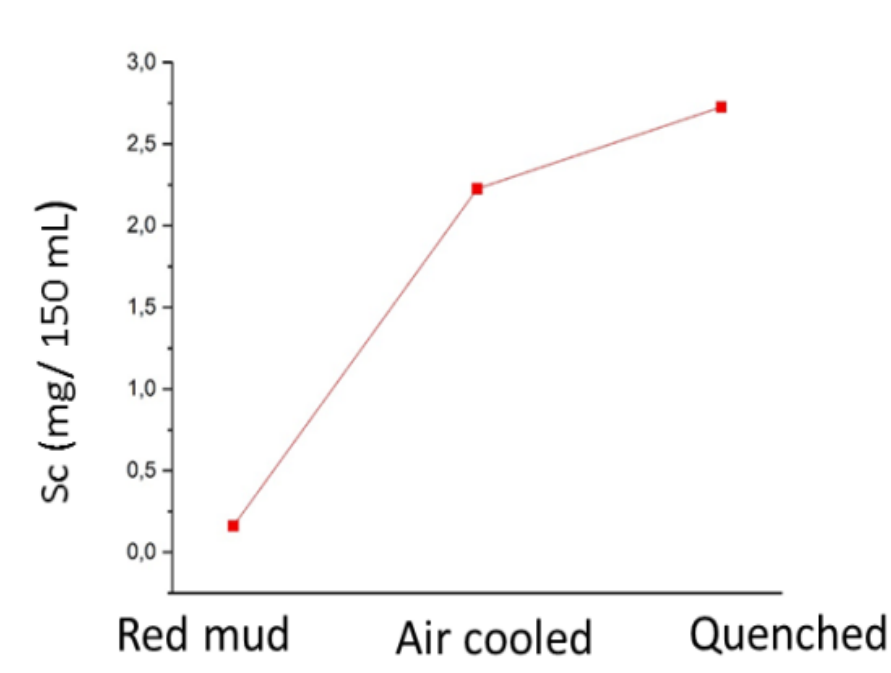
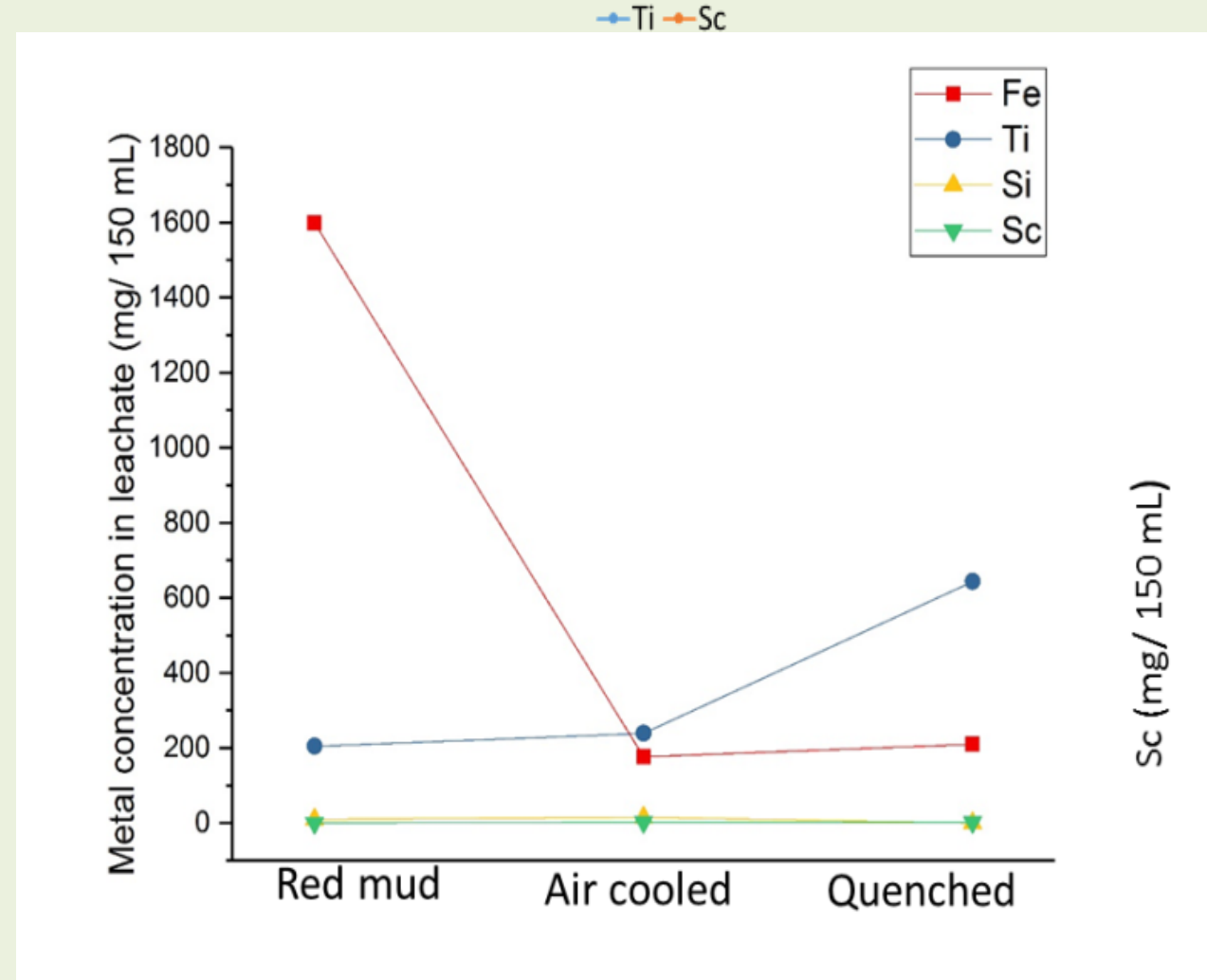
Fe depleted slags and red mud were subjected to acidic leaching; 2.5 M H<sub>2</sub>SO<sub>4</sub>: 2.5 H<sub>2</sub>O<sub>2</sub>, s/l : 1/10, T=75 °C, t=2 h

## Results and Discussion

### Determination of acid molarity



- 1 M ; very poor Ti leaching efficiencies (~ 1 %)
- 2.5 M; slight increase to 20 %
- High amounts of Ca ; calcium sulfate formation that use major sulfate suppress Ti dissolution.
- Low peroxide; gelation tendency was high
- 2.5 : 2.5 is determined to be used**

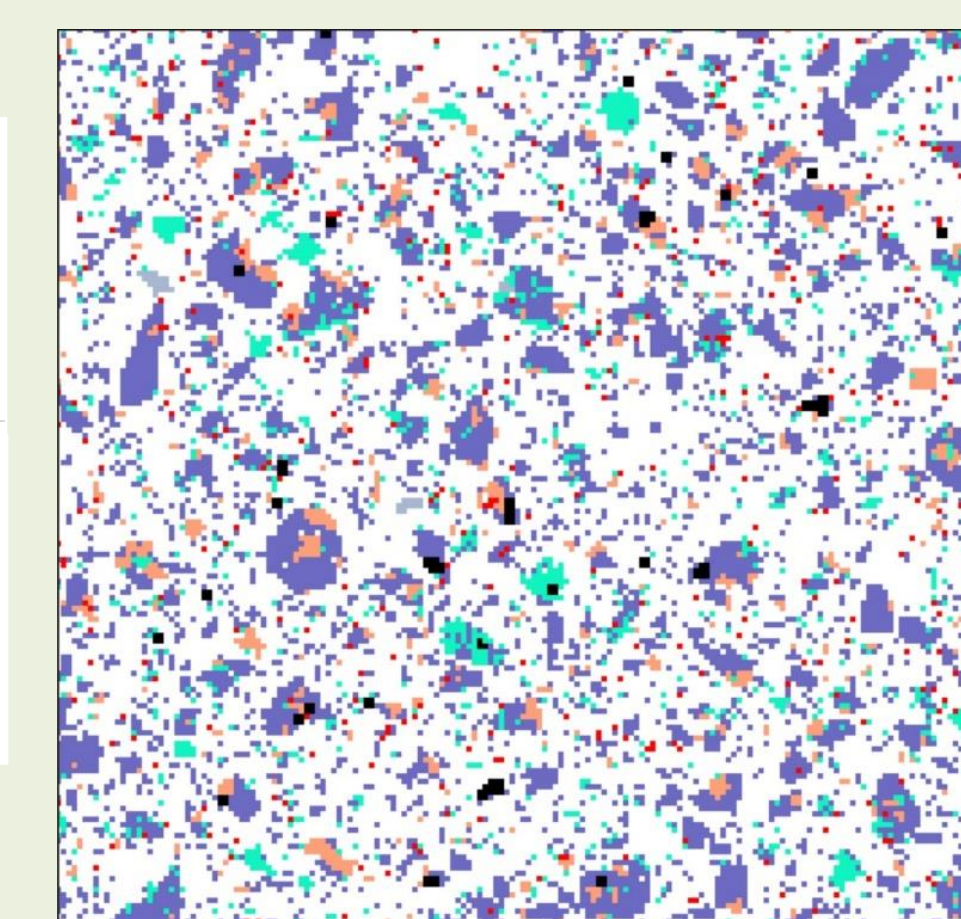
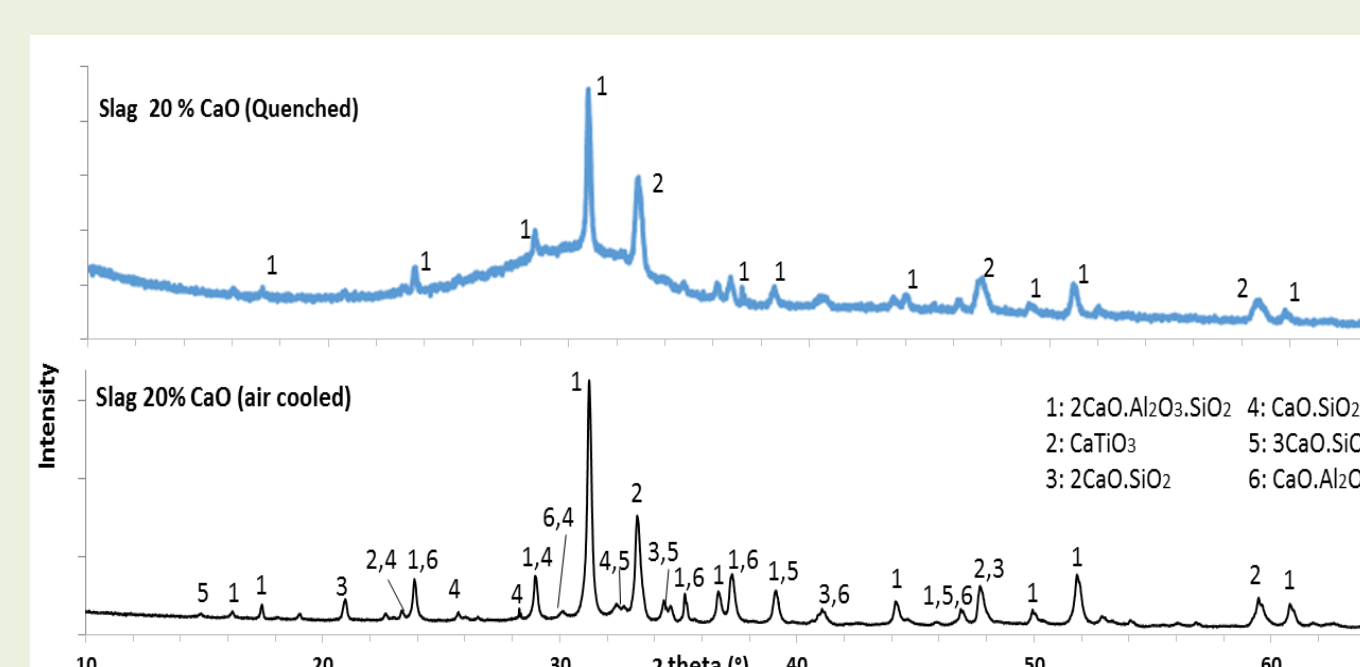


### Comparison of red mud and slags



- Suppressed Ti extraction efficiency in air cooled slag
- Slightly increased Ti efficiency w.r.t. red mud when quenched slag is used; due to less crystalline and easily soluble nature
- High Sc leaching from both slags, especially from quenched ~94 %

### Investigation of slags crystal structure and mineralogy



Mineral	Color
Wustite (S)	Black
Low BSE Hematite (S)	Dark Blue
Magnetite (S)	Dark Blue
Goethite (S)	Dark Blue
Fe-Ca-Al-Silicate	Dark Blue
Gypsum	Dark Blue
Corundum	Dark Blue
Trisulphate	Dark Blue
Quartz	Dark Blue
Pig Feldspar	Dark Blue
Sillimanite (S)	Dark Blue
Kaolinite (S)	Dark Blue
Feld (S)	Dark Blue
Ferrous (S)	Dark Blue
Na-Aluminate	Dark Blue
Ca-Oxide (Cupidine)	Dark Blue
Zircon	Dark Blue
Cpx	Dark Blue
Al2SiO5(OH)4	Light Blue
NaAlO2	Light Blue
Na-Ca-Si-Oxide Ti > 5	Light Blue
Ca-Al-Si-Oxide Ti < 10	Light Blue
Ca-Al-Si-Oxide Ti > 10	Light Blue
Na-Al-Si-F-O	Light Blue
Na-Ca-Si-Oxide Ti > 10	Light Blue
Na-Al-Si-F-O	Light Blue
Rhombohedral	Light Blue
Fe-K Sulphate	Light Blue
Perovskite	Light Blue
Titanium (T)	Light Blue
Silica-Sulphate Gel/Kacke	Light Blue
Silicate	Light Blue
Na-Fe-Al Silicate	Light Blue
Gelignite	Light Blue
Si-Gelignite	Light Blue
Ferri-Gelignite	Light Blue
Iron	Light Blue
Other Minerals	Light Blue
Unclassified (T)	Light Blue

- Metal concentration of PLS highlights almost 3 and 5 folds increase in Ti and Sc: respectively when compared with red mud PLS
- A 10 fold decrease of Fe in leachate indicates selectivity of process.
- For Sc recovery, slag utilization is highly promising

- Quenched slag; poor crystallized with amorphous nature
- Well defined and narrow peaks case of air cooling
- Stable perovskite formation; may be the reason of low dissolution rates
- Perovskite entrapped in CaAl-Si oxide phase

## Conclusions

- Removal of Fe before the acidic leaching step improved significantly the efficiency of Sc leaching (Ariah > 28pt)
- CaO-fed EAF treated and quenched slag followed by H<sub>2</sub>SO<sub>4</sub>: H<sub>2</sub>O<sub>2</sub> leaching, 90% Sc recovery
- Owing to the formation of stable perovskite. poor Ti leaching efficiency
- Sc and Ti enriched PLS after leaching of quenched slag
- Scandium (Sc), can then be further treated with purification operations to synthesize a Sc concentrate

## References

- Wang, W., Pranolo, Y. & Cheng, C. Y. Metallurgical processes for scandium recovery from various resources: A review. Hydrometallurgy 108, 100-108 (2011). Pontikes, Y.I., Maffliet, A. 2011. Process Intensification Routes for Mineral Carbonation. Greenhouse Gases: Science and Technology, 1(4), 287-293.
- Borra, C. R., Pontikes, Y., Binnemans, K. & Van Gerven, T. Leaching of rare earths from bauxite residue (red mud). Minerals Engineering 76, 20-27 (2015). Taylor, H.F.W., 1997. Cement Chemistry. 2nd ed., Thomas Telford Pub., London.
- Alkan, G., Xakalashé, B., Yagmurlu, B., Kaussen, F. & Friedrich, B. Conditioning of red mud for subsequent titanium and scandium recovery—a conceptual design study. World of Metallurgy—ERZMETALL 70, 5-12 (2017)
- Avdibegović, D., Regadio, M. & Binnemans, K. Recovery of scandium (III) from diluted aqueous solutions by a supported ionic liquid phase (SILP). RSC Advances 7, 49664-49674 (2017).

